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## AUTOMATIC SCREW MACHINE PRACTICE

PART VIII

### MILLING, CROSS-DRILLING AND BURRING OPERATIONS

By DOUGLAS T. HAMILTON

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## CHAPTER I

### MILLING ATTACHMENTS

One of the most commonly used milling attachments for the Brown & Sharpe automatic screw machines is the screw-slotting attachment. This attachment, shown at *A* in Fig. 1 is fastened to a boss provided for this purpose on the machine. The apron *B*, which is also an additional part, carries the arbor *C* to which the transferring arm *F* is attached. The transferring and advancing cam levers *D* and *E* are also fastened to bosses on this apron. These levers are operated by the advancing and transferring cams *J* and *K*. The block *H* is fastened to the arm *F*, and a slotting bushing to carry off the screw is

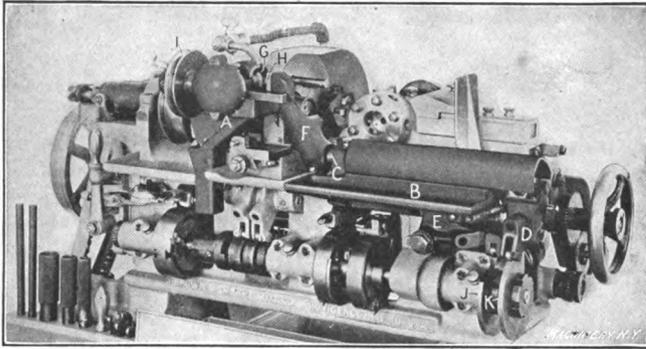


Fig. 1. No. 00 Brown & Sharpe Automatic Screw Machine equipped with a Screw-slotting Attachment

driven into it. This bushing grips the screw and holds it while the slotting saw *G*, held on an arbor and driven from pulley *I* through bevel gears, mills the slot in the head. The pulley *I* is driven by a round belt from the overhead works. The design and action of this device is described in detail in MACHINERY'S Reference Book No. 100, "Automatic Screw Machine Practice—Designing and Cutting Cams for the Brown & Sharpe Automatic Screw Machine," where the laying out of cams for this device is also described.

#### Slotting-bushings

The method of holding the screw when presenting it to the saw in the screw slotting attachment is of special importance. In Table I is shown the standard form of slotting-bushings used for holding fillister- and flat-head screws. The type of slotting-bushing used for round- or button-head screws is similar to that shown for the fillister-head screw, except that in some cases the bushing is not counterbored for the head of the screw. The proportions for slotting-bushings for the

various sizes of Brown & Sharpe automatic screw machines are also given in Table I. The diameter of the hole *A* governs the diameter *B* of the front end of the bushing, and also of the hole *D*. These sizes, of course, pertain only to bushings for standard screws, the slotting-bushing being made to suit the work as desired. The diameter *A* should be made from 0.001 to 0.0015 inch larger than the screw diameter, while the diameter *a* should be made from 0.002 to 0.003 inch larger than the diameter of the shoulder or head of the screw, as the case may be.

When a bushing is to hold a shouldered screw, and when the length of the shoulder is greater than or equal to the diameter of the shoulder,

TABLE I. PROPORTIONS FOR SLOTTING-BUSHINGS

Mch. No.	A	B	C	D	E	F	G	H	I	J
00	$\frac{1}{16}$ to $\frac{3}{16}$	$\frac{3}{8}$	$\frac{3}{8}$	$\frac{1}{2}$	0.450	0.476	$\frac{1}{2}$	$\frac{11}{16}$	$\frac{1}{8}$	1
	$\frac{3}{16}$ to $\frac{1}{2}$	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{5}{8}$	0.450	0.476	$\frac{1}{2}$	$\frac{11}{16}$	$\frac{1}{8}$	1
0	$\frac{1}{2}$ to $\frac{1}{2}$	$\frac{1}{2}$	$\frac{11}{16}$	$\frac{3}{4}$	0.600	0.681	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{1}{8}$	$1\frac{1}{8}$
	$\frac{1}{2}$ to $\frac{3}{4}$	$\frac{11}{16}$	$\frac{11}{16}$	$\frac{3}{4}$	0.600	0.681	$\frac{3}{4}$	$\frac{3}{4}$	..	$1\frac{1}{8}$
2	$\frac{3}{8}$ to $\frac{3}{8}$	$\frac{3}{8}$	$\frac{7}{8}$	$\frac{3}{4}$	0.750	0.792	$\frac{3}{8}$	1	$\frac{1}{8}$	$1\frac{1}{2}$
	$\frac{3}{8}$ to $\frac{1}{2}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{3}{4}$	0.750	0.792	$\frac{3}{8}$	1	..	$1\frac{1}{2}$

the diameter *A* is made to fit the body of the shoulder instead of the body of the threaded part of the screw. When the length of the shoulder is less than the diameter, the bushing is made to fit both the shoulder and the body of the screw. The screw head should also fit in the counterbored hole in the bushing. The distance between the shoulders on the screw should always be less than the distance between the shoulders in the bushing, so that the screw head alone will bear against the shoulder in the bushing. The distance *d* on the bushing for flat-head screws should be made equal to one-half the thickness of the head, when the body of the screw is greater than  $\frac{1}{4}$  inch. When the body of the screw is less than this, the head, as a rule, is usually sunk the full depth in the slotting-bushing. The corner *c* should only be beveled when the diameter of the counterbored hole *A* will permit, otherwise the corner should not be beveled, but rounded slightly.

Slotting-bushings are usually made from tool steel, and are not hardened until the cams have been tried out and the whole equipment is completed. The slot for the ejector is cut before the bushing is inserted in the transferring block, and the slot for the saw in the bushing for flat-head screws is cut when the bushing is held in position in the transferring block. When a bushing is to hold a fillister-head screw, the slotting saw does not, as a rule, touch the bushing at all, the depth of the counterbore  $b$  in the bushing being slightly less than the difference between the depth of the slot and the thickness of the head of the screw. The dimension  $F$  is not taken at the shoulder of the bushing, but is the largest diameter of the taper hole

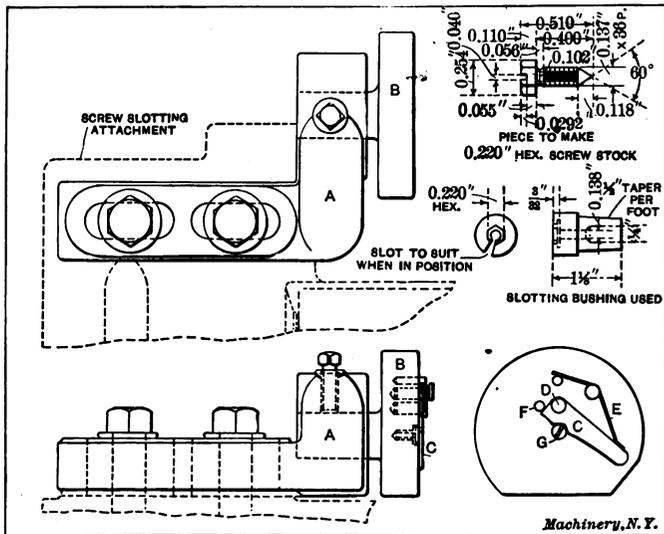


Fig. 2. Device for Locating Hexagon-head Screws in the Slotting-bushing

in the transferring block. This allows the bushing to be driven tightly into the block,  $1/32$  inch being allowed for driving. It is customary, however, to make the dimension  $F$  slightly larger than necessary and fit it into the block when trying out the job. The bevel in the bushing for holding flat-head screws is made to suit the included angle of the head, the angle shown being that adopted by the A. S. M. E.

#### Slotting Hexagon-head Screws

When the slot in the head of a hexagon screw has to bear some definite relation to the sides of the head, it is necessary that the screw be located in an exact position in the slotting-bushing. The bushing for holding the screw has usually an impression in it, which fits the hexagon head, but it is often difficult to get the screw to locate properly in the bushing. If the bushing is forced onto the work when it is attached to the bar, the screw will seldom be correctly located in the hexagon hole, but the corners of the head will be torn off, and the

screw broken off before it is severed from the bar. To obviate this difficulty, some device must be employed for locating the screw in the bushing, after it has been severed from the bar.

A device which is used for locating a hexagon-head screw in the slotting-bushing is shown in Fig. 2, where the screw and slotting-bushing are also shown. This device consists of a cast-iron bracket *A*, which is held on the slotting attachment, being retained in position with the same screws that hold the slotting attachment. Held in the boss of bracket *A* is a holder *B* to which is attached the locator *C*. This consists of a piece of sheet steel about 1/16 inch thick, held on a pin *D* and free to swivel. Pressing against this locator is a spring *E* which forces the locator against the stop pin *F*. A screw *G* acts as a stop, being adjusted in or out as desired to locate the head of the

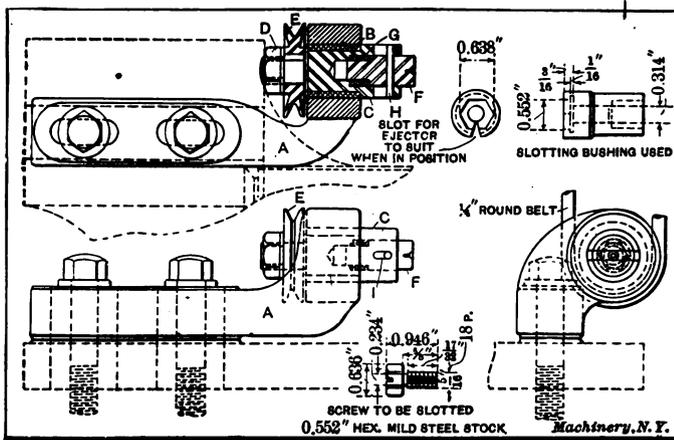


Fig. 3. Another Hexagon Screw Locating Device

screw against the shoulder in the bushing, and also acting as a stop for the locator *C*.

In operation, as the screw is removed from the chuck by the slotting bushing, the arm, in ascending, is brought to dwell in an intermediate position, and is then advanced towards the locator *C*. As this locator is beveled, the screw forces it up, and the action of the spring turns the screw around in the bushing, so that the hexagon head is located properly, the arm at the same time advancing and forcing the screw in to the desired depth. The method of designing the transferring cam to dwell in this intermediate position will be described in connection with the burring attachment, in another chapter.

In Fig. 3 is shown a device for locating hexagon-head screws in the slotting-bushing which differs somewhat in principle from that shown in Fig. 2. This device consists of a cast-iron bracket *A*, which is fastened to the slotting attachment as previously described. The bracket is provided with a phosphor-bronze sleeve *B*, in which a spindle *C* is free to rotate. Keyed to the spindle *C*, and held by a nut *D*, is a

grooved pulley *E*, which is driven by a ¼-inch round belt from the overhead works. Held in the spindle *C* is a spring plunger *F*, which is pressed forward by an open-wound spring *G*. This spring plunger is prevented from rotating by a pin *H*, which fits in an elongated slot *I*, cut in the spindle *C*.

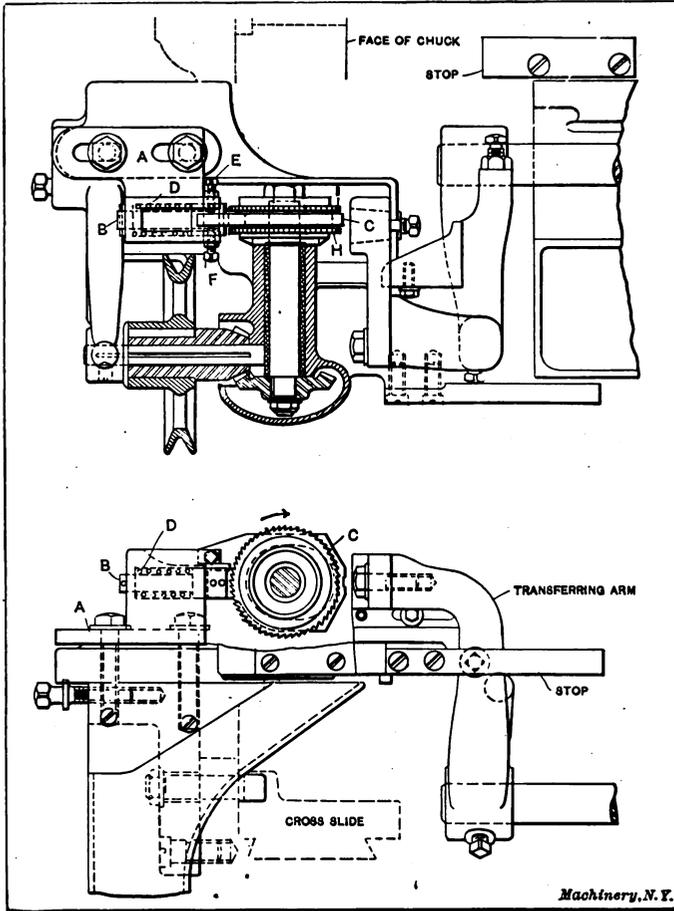


Fig. 4. Slabbing Attachment used on Screw-slottting Attachment

In operation, as the slotting-bushing lifts the screw from the chuck, the arm dwells in an intermediate position, travels forward and presses the screw against the rotating plunger *F*. As this plunger is driven slowly, and as the arm is advanced, the friction between the head of the screw and the plunger rotates the former. On the continued forward travel of the arm, the screw is located correctly in the bushing and forced in to the correct depth. The screw and the slotting bushing

used for holding it are shown in the illustration, where the principal dimensions on the slotting-bushing are also given.

#### Slabbing Attachment

A slabbing attachment which is fastened to the ordinary screw-slotting attachment is shown in Fig. 4. The screws which hold the slotting attachment to the frame of the machine are removed and the slabbing attachment *A* is seated on the top face of the base of the slotting attachment. The screws are again inserted, and the slabbing attachment fastened in position. The main body of the attachment is an iron casting, and a boss on it is bored out to receive a plunger *B* to which is attached a guide or ejector *C*. The plunger *B* is riveted to this guide member *C*, and a coil spring *D* is located behind the shoulder of the plunger to keep it out.

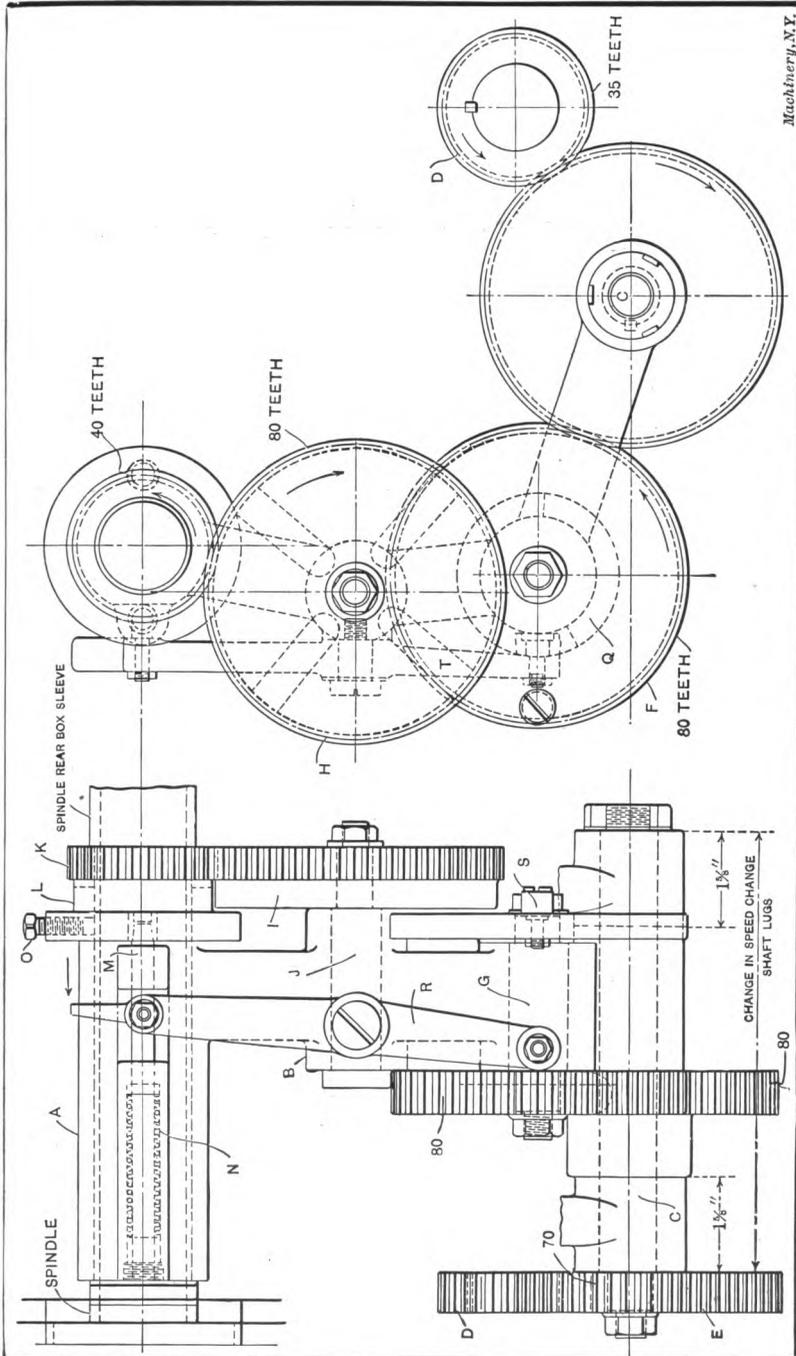
Two set-screws *E* and *F* with lock-nuts are provided for guiding the member *C*. This guiding or ejecting member *C* has an elongated hole bored in it, fitting over the saw arbor, so that the ejector can be forced back by the piece when it is being advanced to the slabbing saws by the transferring arm. The front face of the ejector *C* is knurled, so that the piece is prevented from rotating in the slotting-bushing when the saws *H* and *I* commence to cut. This attachment is driven in the same manner as the ordinary screw-slotting attachment, and the bushing in which the work is held while being slabbed is also of a similar type. Of course, the exact shape of the bushing would depend entirely on the shape of the work. In the lower view, the driving mechanism has been removed to show the slabbing attachment more clearly.

#### Spindle Indexing Device

A device which converts the Brown & Sharpe automatic screw machine into a milling machine is shown in Fig. 5. This device was designed for making a special piece, which is shown at *A* in Fig. 6, where the cams for making the piece are also shown.

To apply this device to the automatic screw machine, the pulleys *A* and *B* shown in Fig. 7 are removed, as is also the clutch mechanism. The outer sleeve *A* of the attachment shown in Fig. 5 is then slipped over the regular spindle. This sleeve is cast integral with a bracket *B*, the lower end of which is located on the shaft *C* shown in Fig. 7. This shaft is part of the belt-shifting arrangement which is used for obtaining two different speeds for the spindle when threading steel. The attachment is driven from the rear driving-shaft by the ordinary gears *D* and *E* which drive the belt-shifting arrangement as shown in Figs. 5 and 7. A 35-tooth gear *D* is placed on the driving shaft, which meshes with a 70-tooth gear *E* located on the shaft *C*. On the same shaft is an 80-tooth gear driving an 80-tooth gear *F* on the stud *G*.

A trip and indexing mechanism somewhat similar to that used on the turret, is used here for indexing and locking the spindle. The 80-tooth gear *H* meshes with a 40-tooth gear *K* keyed to the sleeve *L* held on the spindle. This sleeve has two holes drilled in it, in which the plunger *M* fits. A spring *N* behind this plunger keeps it in contact



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Fig. 5. Attachment for Indexing the Main Driving Spindle of a Brown & Sharpe Automatic Screw Machine

with the sleeve *L*. This sleeve *L* is fastened to the main driving-spindle of the machine by a set-screw *O*. This attachment is operated as follows:

The dog on the drum held on the front cam-shaft, is set to trip the lever, which, when tripped, operates the tooth-clutch *P*. Fig. 7, thus rotating the rear driving-shaft. As the rear driving-shaft rotates at 180 R. P. M., the gear *D* will revolve at the same speed, while the gear *E* will revolve at 90 R. P. M., and will transmit a speed of 90 R. P. M. to the gear *F*. This gear *F* carries a cam *Q*, and a roller attached to

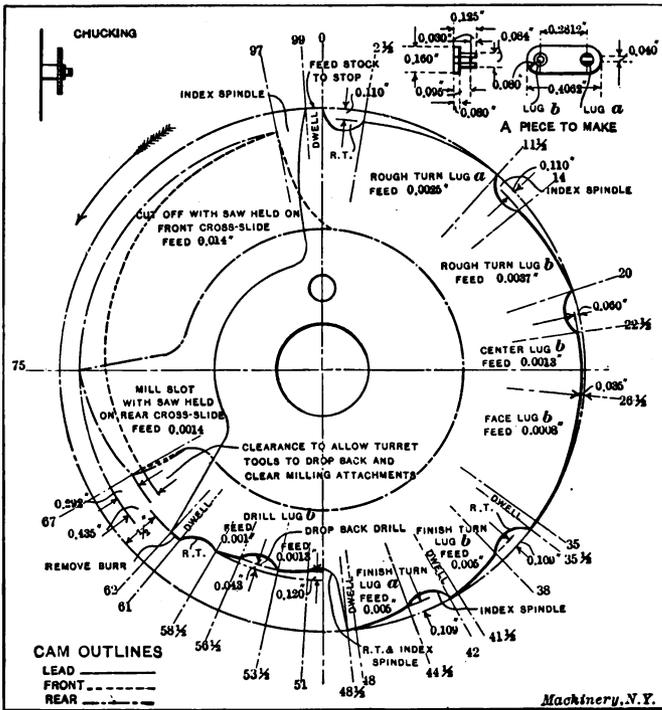


Fig. 6. Lay-out of a Set of Cams for Making a Piece requiring the Indexing of the Work-spindle

the lever *R* runs on this cam. Then when the dog trips the lever, the driving-shaft rotates, thus driving the gears, which in turn rotate the cam *Q*. As the cam *Q* is rotated, the arm *R* is moved in the direction indicated, which action withdraws the pin *M* from the bushing *L*. Now at the same time that the pin *M* is withdrawn, the roller *S* comes in contact with the slot *T* in disk *I* held on the stud *J*, thus rotating the disk on one quarter turn. This disk is provided with four slots *T*, and as this indexing device requires to be indexed 180 degrees to bring each part of the piece into position, the disk *I* is moved two spaces before another dog on the drum trips the lever that disengages the tooth-clutch *P*, Fig. 7.

Referring to Fig. 6, it will be seen that the piece to be made has two lugs on it designated *a* and *b*. The stock from which this piece is made is of special shape, so that its outside circumference does not require to be finished; the lugs *a* and *b* are to be formed, drilled and slotted. The work is not revolved, but is only indexed to bring the stock into position for forming the two lugs. To turn these lugs, the turret is packed out an amount equal to one-half the distance between the center of the two lugs, and drilling attachments are used in the turret for holding hollow mills and drills. The order of operations is as follows:

Order of Operations	Revolutions	Hundredths
Feed stock to stop.....	4½	1
Revolve turret .....	12	2½
Rough turn lug <i>a</i> with hollow mill held in drilling attachment, speed 684 R. P. M. at 0.0025 inch feed .....	43	9
Index spindle and revolve turret.....	12	2½
Rough turn lug <i>b</i> with hollow mill held in drilling attachment, speed 684 R. P. M. at 0.0037 inch feed .....	28	6
Revolve turret .....	12	2½
Center and face lug <i>b</i> with centering tool held in drilling attachment, speed 684 R. P. M. at 0.0013 inch feed to center and 0.0008 inch feed to face .....	62	13
Revolve turret .....	12	2½
Finish turn lug <i>b</i> with hollow mill held in drilling attachment, speed 684 R. P. M., at 0.005 inch feed .....	19	4
Index spindle .....	12	2½
Finish turn lug <i>a</i> with hollow mill held in drilling attachment, speed 684 R. P. M., at 0.005 inch feed .....	19	4
Revolve turret and index spindle.....	12	2½
Drill hole in lug <i>b</i> with drill held in drilling attachment, speed 3555 R. P. M. at 0.0013 inch feed .....	12	2½
Pull out drill to remove chips.....	14	3
Finish drill hole in lug <i>b</i> with drill held in drilling attachment, speed 3555 R. P. M., at 0.0011 inch feed .....	9	2
Revolve turret .....	12	2½
Remove burr and broach with tool held in floating holder .....	4½	1
Clear .....	24	5
Mill slot in lug <i>a</i> with special milling attachment held on rear cross-slide, speed 400 R. P. M., at 0.014 inch feed.....	(26)	(8)
Cut-off with special milling attachment held on front cross-slide, speed 480 R. P. M., at 0.014 inch feed .....	143	30
Index spindle .....	10	2
	476	100

## Cross-slide Slotting Attachment

The special slotting attachment designed for cutting the slot in lug *a* shown in Fig 6 is shown in Fig. 8. This attachment consists of a block *A*, the base of which is held to the rear cross-slide by a bolt and

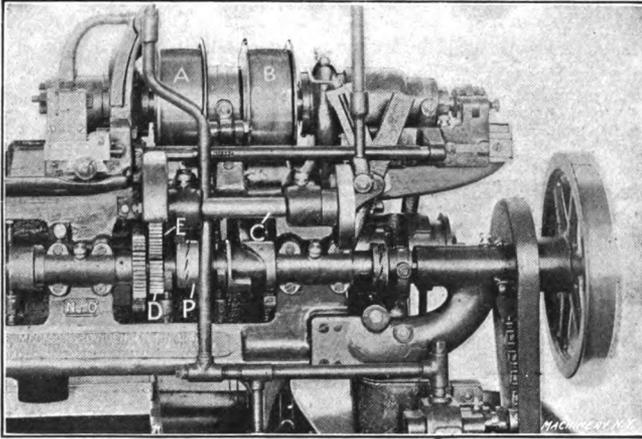


Fig. 7. Illustration showing the Location of the Indexing Attachment

nut *B* and *C* as shown, the former fitting in the T-slot in the cross-slide. The spindle *D* passing through the casting which is bushed with a bronze sleeve, has attached to it a bevel gear *E*, meshing with a

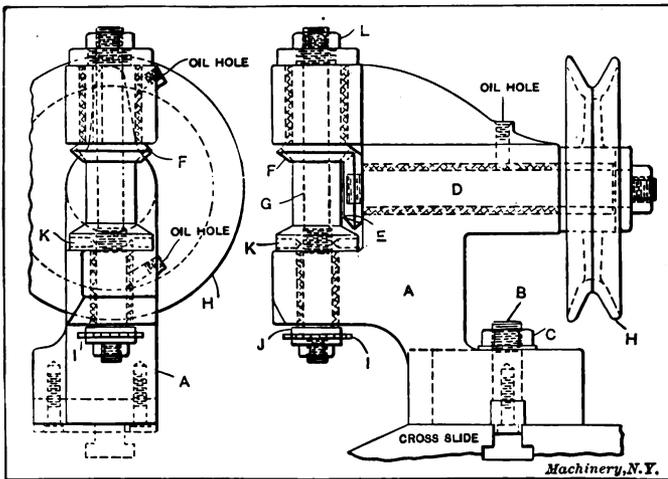


Fig. 8. Slotting Attachment held on the Rear Cross-slide

bevel gear *F* keyed to the vertical spindle *G*. This vertical spindle *G* also runs in bronze bushings. The pulley *H* is keyed to the rear end of shaft *D* and is held to it by a nut and washer as shown. A round belt which passes over a grooved pulley held on the countershaft,

drives this pulley *H*, which, in turn, drives the slotting saw *I* held on the lower end of the vertical spindle. Adjustment is provided for the slotting saw *I* by varying the thickness of the washer *J* and also by means of the adjusting nuts *K* and *L*. Gear *F* has a shank which fits in the upper member, so that the spindle *G* can be adjusted without affecting the position of this gear.

#### Cross-slide Sawing Attachment

The attachment which is used for cutting off the piece shown at *A* in Fig. 6 is shown in Fig. 9. This attachment is held on the front

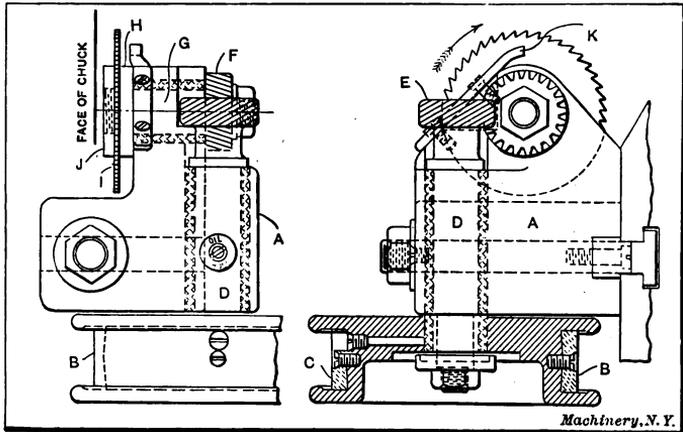


Fig. 9. Sawing Attachment held on the Front Cross-slide

cross-slide, and consists of a holder *A* somewhat similar to the ordinary holder used for the circular form tools, and is also held to the cross-slide in a similar manner. A three-quarter inch flat belt, which passes over a pulley fastened to the countershaft, drives this attachment through the pulley *B*. This pulley *B* has a leather strip *C* fastened to it which increases the friction and gives a more positive drive to the cutting-off saw. The pulley *B* is keyed to a shaft *D*, and also held to it by a nut and washer as shown. The shaft *D* which passes through a bronze bushing held in the holder *A* has a helical gear *E* cut on its forward end. This helical gear meshes with a mating gear *F* held on the cutter spindle *G*, which is located at right angles to the spindle *D*. The spindle *G* fits in a bronze sleeve held in the holder *A*, and is provided with a shoulder *H* against which the slotting saw *I* is held by the nut *J*. The guard *K* is used to prevent the work from springing away from the saw when almost cut off.

## CHAPTER II

### CROSS-DRILLING ATTACHMENTS

In order to avoid a separate operation in manufacturing parts requiring to be cross-drilled, the Brown & Sharpe Mfg. Co. has designed what is called an "index drilling attachment." This attachment, which is used for drilling cross-holes in studs and capstan-screws, is illustrated in Figs. 10, 11 and 12.

The Brown & Sharpe index drilling attachment, which is shown located on a No. 00 automatic screw machine in Figs. 10 and 11, consists mainly of a cast-iron bracket *A*, fastened by cap-screws to a boss

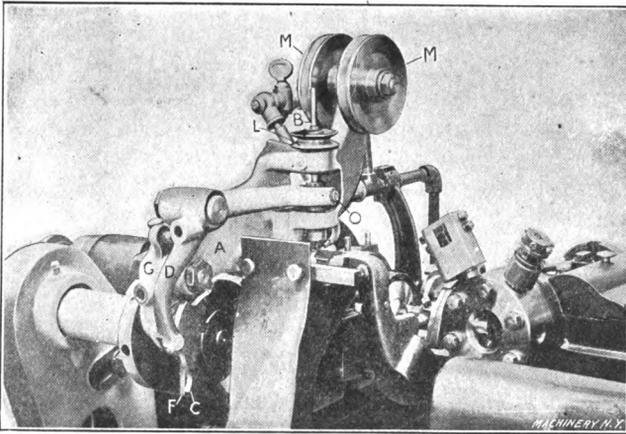


Fig. 10. Front View of the Index Drilling Attachment, placed on a No. 00 Brown & Sharpe Automatic Screw Machine

provided for that purpose on the machine. In this bracket are held the work- and drilling-spindles, the latter being held in a vertical position and in line with the work-spindle. The camshaft from which the attachment is operated, is driven by a chain and sprocket, which is shown encased in Fig. 10. A sprocket-wheel for driving the attachment is placed on the front camshaft of the machine, and an idler pulley, fastened to a bracket, gives the chain the desired tension on the sprocket. Figs. 10 and 11 give a general idea of the construction of this index drilling attachment, but for a more detailed description reference should be made to Fig. 12. Similar parts in the three illustrations bear the same reference letters.

The drilling-spindle *B* is driven by a  $\frac{3}{8}$ -inch round belt from the overhead works through pulleys *L* and *M*, the pulleys *M* acting as idlers, to change the direction of the belt from a vertical to a horizontal position. Spindle *B* is operated by a cam *C* acting through a lever *D*,

while the indexing of the work-spindle *E* is accomplished by a cam *F* acting through a lever *G*. The forward end of the lever *G* has teeth cut in it (see Fig. 18) which mesh with the segment gear *H* on the work-spindle *E*, Fig. 12. A ratchet *I*, held to the segment gear by a shoulder screw and nut as shown, and acted upon by a spring, fits in a ratchet disk *I*, (see Fig. 18) which is keyed to the work-spindle *E*. The locking plate *J* has V-notches cut in it, the number of which (usually four) equals the indexings of the spindle required, this plate being used for locking purposes only. A spring plunger *K* fits in the notches in plate *J* and holds it in place until the spindle is again indexed.

In operation, when the indexing lever *G* is raised by the cam *F*, it depresses the spring plunger *N*, and at the same time rotates the seg-

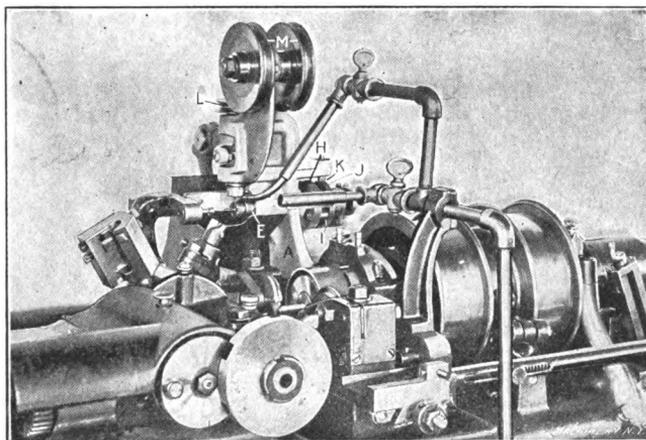


Fig. 11. Rear View of the Index Drilling Attachment in Place on a No. 00 Brown & Sharpe Automatic Screw Machine

ment gear *H* carrying the ratchet *I*. The spring plunger returns the lever to its normal position when the roll on the lever drops down to the smallest diameter of the cam, and in so doing returns the indexing disk *H* to its normal position ready for the next indexing. The work-spindle is indexed by the ratchet *I* meshing in one of the teeth in the ratchet disk *I*.

The drilling-spindle *B* is raised and lowered by means of the lever *D*, which is connected to it by two screws *O*, holding two shoes, the latter fitting in milled slots cut in the sleeve *P*. This sleeve is held on the spindle *B* by check-nuts *Q*. The drill-spindle runs in bronze bearings, and is provided at its lower end with three set-screws *R* for holding the drill. The upper end of the drill-spindle fits in a steel bushing *S*, to which it is keyed. The pulley *L* is also keyed to bushing *S*, and as the spindle *B* is provided with a groove, it is possible to rotate the spindle, and at the same time move it up and down by the lever *D*.

A general outline of the construction of the various details of the attachment is given in the following:

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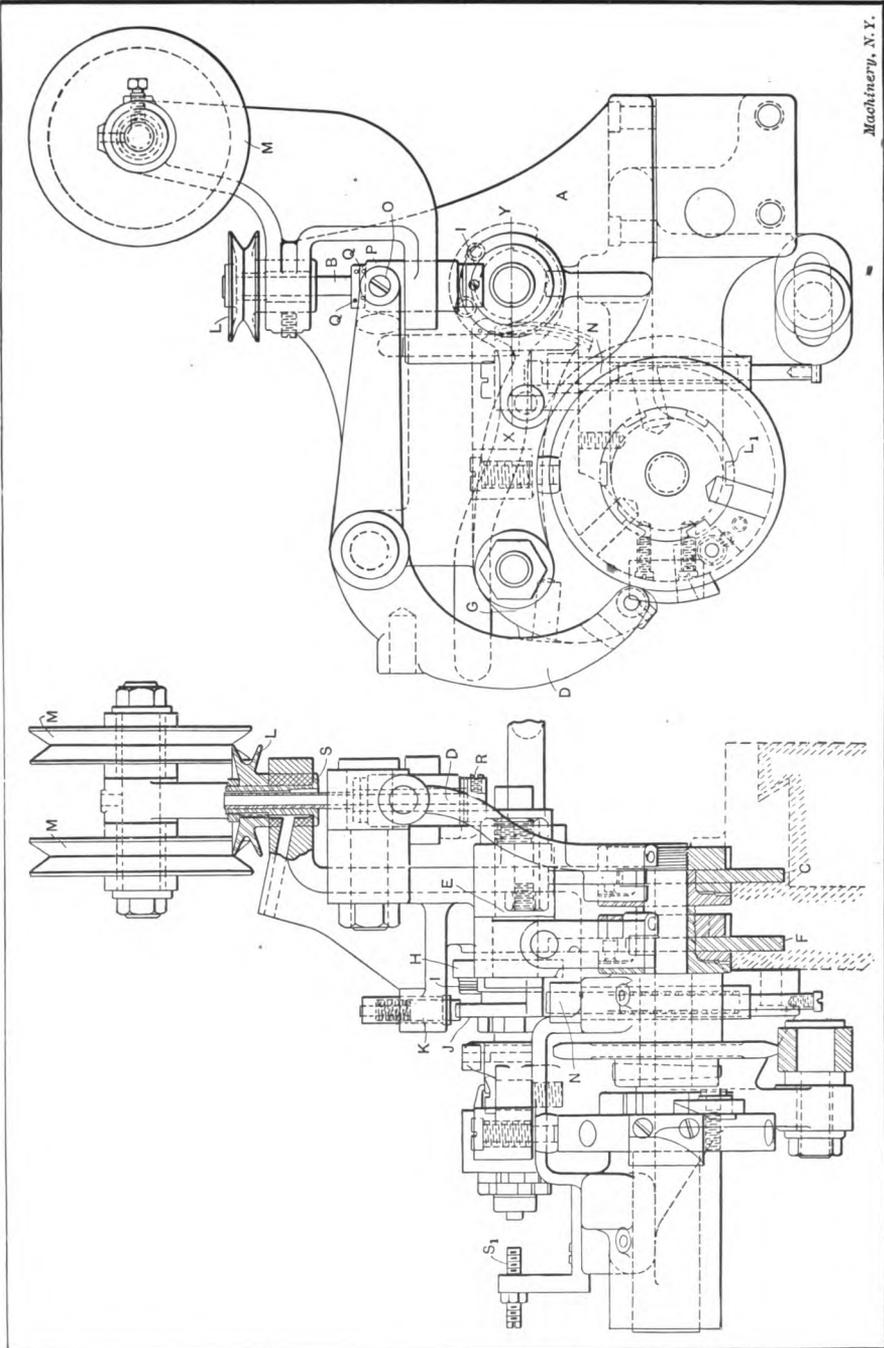


Fig. 12. Assembly View of the Index Drilling Attachment for the No. 00 Brown & Sharpe Automatic Screw Machine

## Construction of the Index Work-spindle

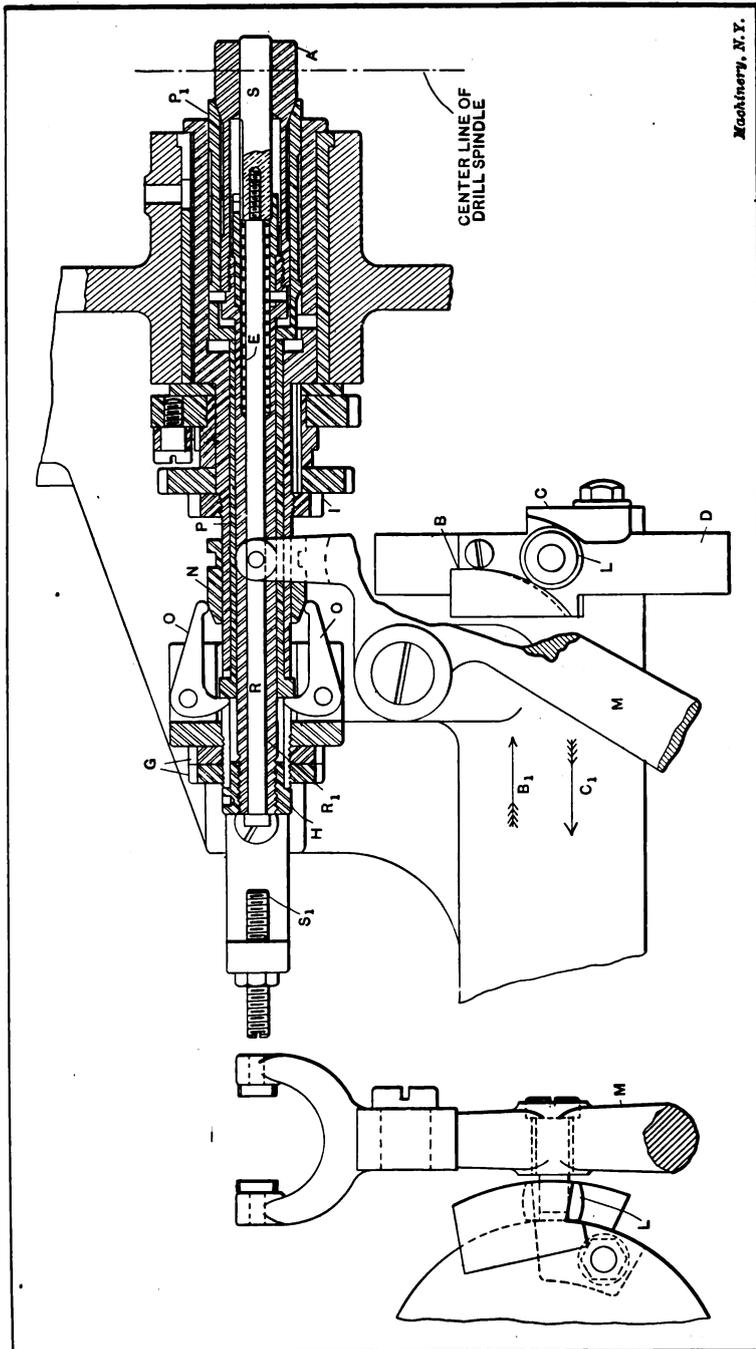
Fig. 13 shows a sectional view of the index work-spindle, the section being taken on the line *X-Y*, Fig. 12. The spindle, as has been previously stated, is indexed, but otherwise remains stationary. The chuck *A* is closed by means of the cam *B*, which is fastened by screws to the drum *D*, while the cam *C* operates the lever *M* for opening the chuck. A roller *L*, attached to the lever *M*, and which is guided by the cam-blocks *B* and *C*, operates the lever *M* for closing and opening the chuck.

In operation, as the lever *M* is forced by the cam *C* in the direction indicated by the arrow *C*<sub>1</sub>, it withdraws the clutch sleeve *N* from beneath the fingers *O*, allowing the latter to drop and release their pressure on the sleeve *P*. Now, as the mouth or front end of the sleeve *P*<sub>1</sub> is beveled to an angle which is greater than the angle of repose, and as the chuck *A* is split and spring-tempered, the withdrawal of the clutch sleeve *N* from beneath the fingers *O* allows the bevel on the chuck to force the sleeve *P* back, thus permitting the chuck to open and the work to be ejected by the plunger *S*. Inversely, as the lever *M* is forced by the cam-block *B* in the direction of the arrow *B*<sub>1</sub>, the clutch sleeve *N* is forced under the fingers *O*, so that their circular bearings or ends rest on the straight cylindrical portion of the sleeve. This action on the fingers *O* causes the sleeve *P* to be pushed forward and butt against the sleeve *P*<sub>2</sub>, forcing it over the tapered portion of the chuck *A*, and thus closing the latter on the work.

The work, when forced into the chuck *A*, butts against a brass ejector or stop *S* which is screwed onto the rod *R*. This rod passes entirely through the spindle *R*<sub>1</sub>, and is held outward by a coil spring *E*. When the work forces the ejector *S* into the chuck, the head on the rod *R* comes against the stop-screw *S*<sub>1</sub>, which is clamped by the lock-nut shown. The position of the stop-screw governs the distance to which the work can be inserted in the chuck, thus locating the position of the drilled holes. The desired grip of the chuck *A* on the work is obtained by adjusting the check-nuts *G*. The work-spindle can be taken out by removing the nuts *H* and *I* and the lever *M*.

## Laying out Cross-slide Cams for Cross-drilling Operations

The method of laying out a set of cams for a cross-drilling operation is similar to that for any other job, except that there are a number of special points to be considered which relate chiefly to the clearance allowances for the transferring arm in its ascent and descent to and from the work-spindle. Possibly the best way to illustrate the method employed is to take a practical example and describe each step. Assume that it is required to make the piece shown at *A* in Fig. 14, which is a binding post, made from 9/32-inch brass rod. The turret and cross-slide cams, also shown in this illustration, are laid out in the usual manner, except that sufficient space is allowed, as shown from 86 to 91 (on the cam circumference) for bringing down the transferring arm to grip the work. One hole should be left vacant in the turret, so that the transferring arm can be brought down without coming in contact with any of the turret tools.



Machinery, N. Y.

Fig. 18. Sectional View of the Index Drilling Work-spindle

Before laying out the lead and cross-slide cams, it is preferable to make a lay-out as shown in Fig. 15, drawing in the position of the circular form and cut-off tools and also the tools used in the turret. If this is done, the amount that the cams are to be cut down below the largest diameter of the cam circumference, and also the clearances necessary for the turret and circular form tools, can be found. After the necessary information has been obtained from this diagram, another diagram, such as in Fig. 11, Reference Book No. 100, "Designing and Cutting Cams for the Brown & Sharpe Automatic Screw Ma-

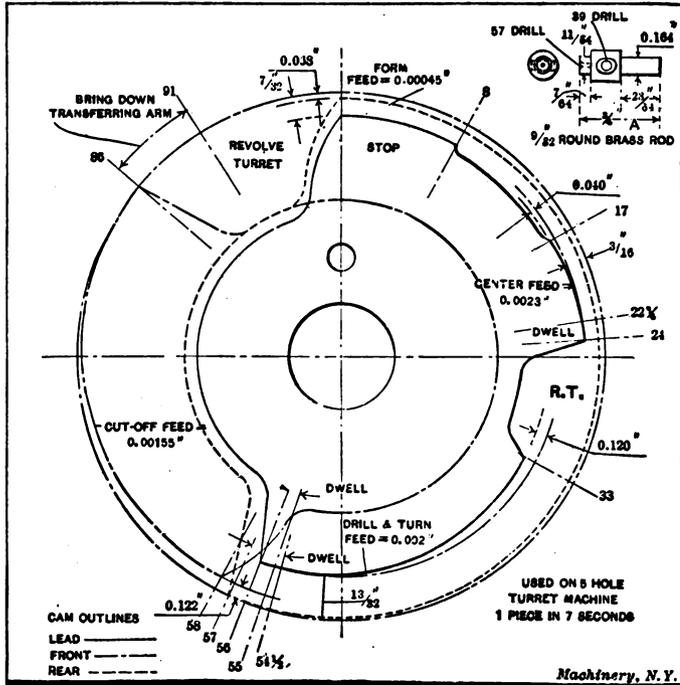


Fig. 14. Lay-out of a Set of Cams for a Cross-drilling Operation on the No. 00 Brown & Sharpe Automatic Screw Machine

chines," should be made so that the rises and the cut-downs on the transferring and advancing cams can be obtained. Of course, the example given in that illustration applies more particularly to a screw-slotting job; the method of procedure, however, for laying out the cams used on the index drilling attachment is similar.

**Laying out the Transferring and Advancing Cams**

As the method of laying out the transferring and advancing cams is described in Part II of this treatise, MACHINERY'S Reference Book No. 100, it will not be necessary to describe it here. The drawing of the transferring and advancing cams used in connection with the piece shown at A in Fig. 14, is shown in Fig. 16. Here the lobes and their



**Lead and Cross-slide Cams**

Order of Operations	Revolutions	Hundredths
Feed stock to stop and chuck,.....	22.40	8
Revolve turret .....	25.20	9
Center 0.040 inch rise at 0.0023 inch feed, dwell 0.125 .....	19.60	7
Revolve turret .....	25.20	9
Drill and turn with box-tool 0.120 inch rise at 0.002 inch feed, dwell 0.15.....	64.40	23
Form with circular tool 0.058 inch rise at 0.00045 inch feed, dwell 0.25.....	(159.60)	(57)
Clearance .....	5.60	2
Cut-off 0.122 inch rise at 0.00155 inch feed, and revolve turret .....	78.40	28
Clearance for transferring arm .....	14.00	5
Revolve turret .....	25.20	9
<b>Total .....</b>	<b>280.00</b>	<b>100</b>

**Transferring and Advancing Cams**

Order of Operations	Revolutions	Hundredths
Place transferring bushing on work.....	11.2	4
Drop arm back from work.....	5.6	2
Lift up transferring arm .....	20.2	7¼
Clearance .....	2.8	1
Dwell with transferring arm while placing work in chuck and drilling .....	187.6	67
Place work in index drilling chuck.....	21.0	7½
Dwell with arm while closing chuck.....	11.2	4
Drop back arm .....	14.0	5
Dwell with arm while drilling.....	131.6	47
Drop down transferring arm to pick up piece..	30.8	11
Clearance .....	2.8	1
Advance to put bushing on work.....	11.9	4¼

**Drilling and Indexing Cams**

Order of Operations	Revolutions	Hundredths
Drill and countersink 0.218 inch rise at 0.0017 inch feed, dwell 0.10.....	127.4	45½
Lift out drill .....	9.1	3¼
Push down lever to index.....	11.2	4
Dwell to allow spring to return lever.....	4.9	1¾
Index second time .....	22.4	8
Dwell to allow spring to return lever.....	4.9	1¾
Clearance .....	9.1	3¼
Countersink 0.062 inch rise at 0.0031 inch feed, dwell 0.10 .....	22.4	8
Pull out drill, open chuck, and allow clearance, ' to drop and raise transferring arm and close chuck .....	65.8	23½

Referring to Fig. 17, it will be seen that the indexing cam is provided with two projecting lobes *B* and *C*, which are used to force the

lever down and thus rotate the indexing disk. These two lobes are necessary because the piece to be drilled has only one cross-hole countersunk on both sides, which necessitates indexing the spindle four times for each piece. Since the indexing and drilling cams rotate at the same speed as the turret and cross-slide cams, the time required for indexing is approximately equal to the time required for feeding the stock, which can be verified by referring to the illustration, the space required being from 61 to 69. Three hundredths of the cam surface is the minimum space which should be allowed, on account of the rolls requiring that space to drop down. A milling cutter at least 1/16 inch larger in diameter than the roll should be used for cutting

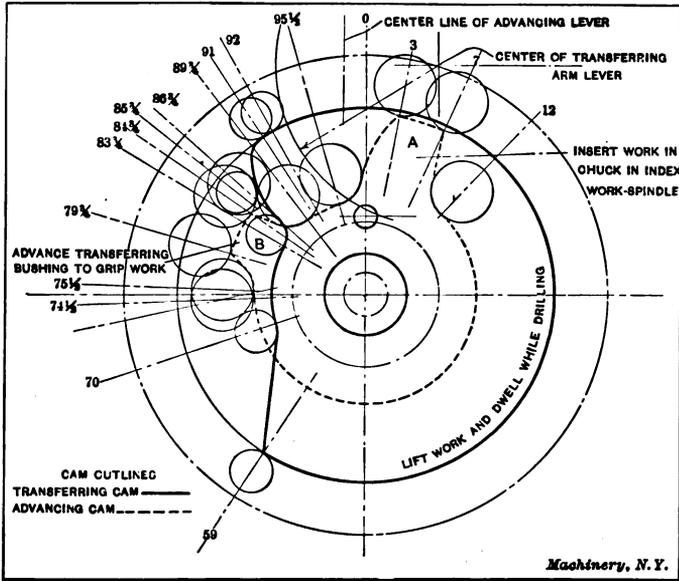


Fig. 16. Transferring and Advancing Cams for Lifting and Placing the Work in the Index Drilling Chuck

the cams. The motion transmitted by the cams to the indexing and drilling levers *G* and *D* is clearly shown by the full and dotted lines in Fig. 18. The maximum travel of the index drilling spindle is equal to the distance *A*, which on the attachments used is as follows:

No. of Machine	Distance A in Inches
00 .....	9/16
0 .....	3/4
2 .....	13/16

The maximum diameters of the indexing and drilling cams for the attachments used on the various machines are as follows:

No. of Machine	Distance B in Inches
00 .....	4
0 .....	4 1/2
2 .....	4 1/2

The cut-down required on the cam for indexing can be found by laying out a diagram similar to that shown in Fig. 18. When the indexing disk  $I_1$  is provided with six teeth instead of four, the cut-down required will be, of course, proportionately less.

#### Speeds and Feeds for Cross-Drilling

The speeds and feeds used for cross-drilling do not vary from those used when drilling from the turret, and to obtain the required speed for the drill a grooved pulley of suitable size should be placed on the

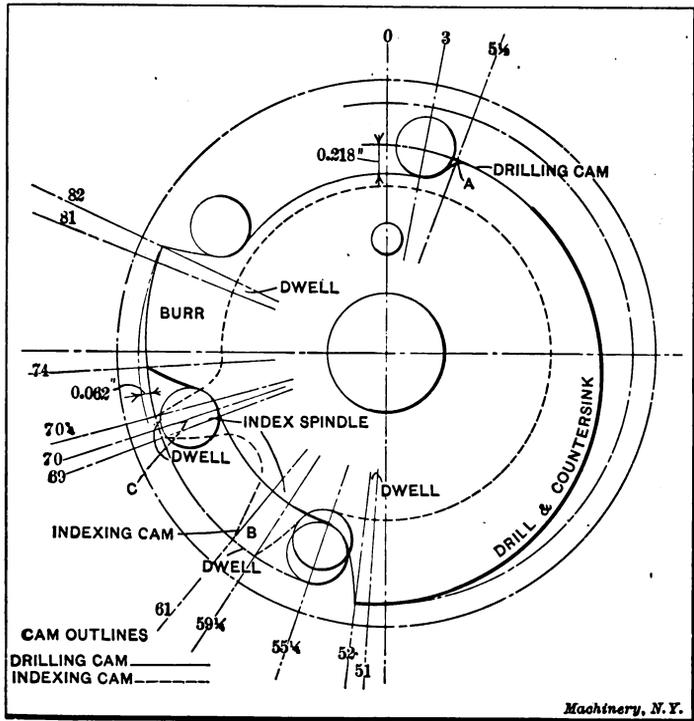


Fig. 17. Indexing and Drilling Cams for the Piece shown at A in Fig. 14

countershaft. The drilling speeds and feeds for ordinary carbon and high-speed twist drills for drilling different materials are given in MACHINERY'S Reference Book No. 103, "Internal Cutting Tools for the Brown & Sharpe Automatic Screw Machines."

#### Transferring Bushings

When transferring a piece of work from the work-spindle to the index drilling spindle, it is necessary to have a transferring bushing which will insert the work in the index drilling chuck. The ordinary screw-slotting bushing cannot be used for this purpose, except when the work is sufficiently long and the hole in a suitable place, so that the work can be inserted in the chuck without the aid of a spring

plunger. When the work is not of the character specified, it is necessary to use a transferring bushing in which is placed a spring plunger for inserting the work in the index drilling chuck.

At *A* in Fig. 19 is shown a capstan-screw and the transferring bushing used for inserting it in the index drilling chuck. This screw, as shown, has two holes drilled clear through the head at right angles to each other. The transferring bushing consists of a shell *a* which is held in the transferring block. Inserted in this shell is a spring plunger *b*, pressed outward by a coil spring *c*, this coil spring being retained in the bushing by means of the nut *d*. The hole in the spring

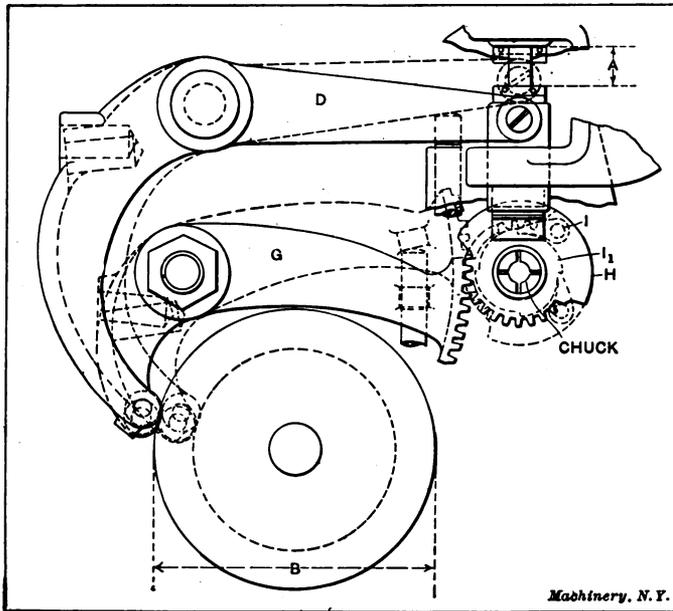


Fig. 18. Diagram illustrating the Movement of the Indexing and Drilling Levers

plunger should be larger in diameter than the body of the screw, so that the work can be inserted easily into the plunger. The type of transferring bushing shown at *A* is suitable for capstan-screws and similar work.

Another transferring bushing for holding a binding post is shown at *B*. This bushing differs from that shown at *A* in that it is provided with a spring chuck as well as with a plunger. The reason for this was that the piece had to be inserted in the chuck to such a distance that it was necessary for the chuck *e* to retreat so that the work could be inserted. This transferring bushing was not a success on account of this combination arrangement of spring chuck and plunger. Difficulty was encountered with the spring chuck *e*, because of the variations in the diameter of the stock. When the stock was much

greater in diameter than the hole in the chuck, the chuck was forced back into the holder so that the work was not held, as the plunger *f* kept it out.

Owing to the short amount of grip on the work, it had to fit snugly in the bushing, or it would drop out while being transferred from the work chuck to the index drilling chuck. To overcome this difficulty several methods were adopted. First, the spring *g* was made stiffer, so that when work slightly larger than the hole in the chuck was encountered, it could be inserted without pushing back the plunger. This

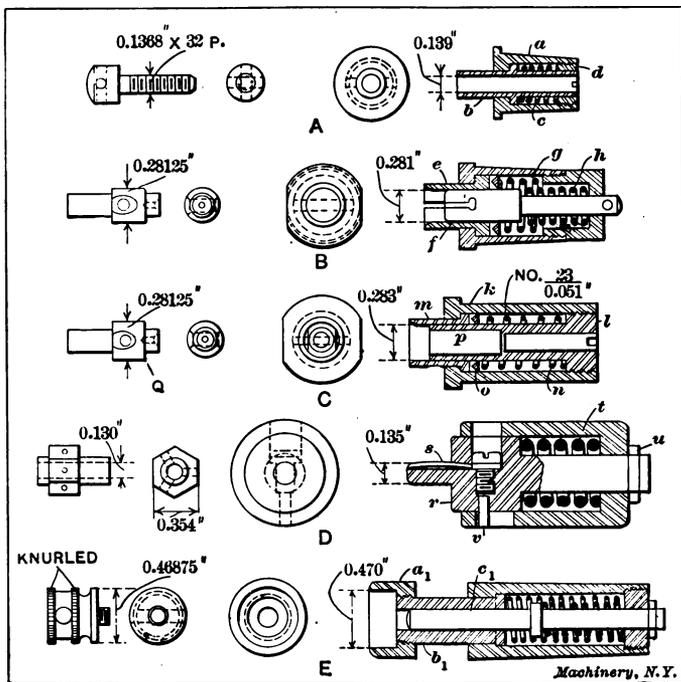


Fig. 19. Representative Types of Transferring Bushings and the Work they were designed to hold

overcame the difficulty of placing the work in the chuck *e*, but when the latter was transferred to the index drilling chuck, the work could not be ejected from the chuck. The spring *h* was made stiffer, but this brought about the same conditions as before, and prevented the work from being located properly in the chuck *e*.

This type of bushing was finally discarded and the one shown at *C* was adopted. This bushing consists of an outer sleeve *k*, as before, in which is screwed a stationary holder *l*. A chuck *m* is made a sliding fit on holder *l*, and also in the sleeve *k*, and is pressed outward by a spring *n*. This spring acts against a washer *o*, which is beveled, as shown, to reduce the friction, thus preventing the spring from being twisted in the holder when work of larger diameter than the chuck is

encountered, causing the chuck to rotate. The hole  $p$  in the holder is made slightly larger than the diameter  $Q$  on the work, while the hole in the bushing  $m$  is made slightly larger than the largest diameter of the work. The holder  $l$  is slabbed on both sides on the front end, as shown in the end view, and the index drilling chuck is cut out so that this holder can be inserted in it, thus carrying the work right into the chuck. This bushing proved very satisfactory, both as regards gripping the work and inserting it in the chuck, and was used on the piece shown at  $A$  in Fig. 14.

A transferring bushing of a different type is shown at  $D$ . This bushing, instead of passing over the work, has a plunger  $r$  which is inserted in a hole in the work. This plunger is slotted, as shown, and a flat spring  $s$  is held to it by a screw. Spring  $s$  is curved and rounded so that it fits snugly in the work. The plunger  $r$  is held out by a coil spring  $t$ , and is retained by a pin  $u$ . A small pin  $v$ , driven into the plunger and fitting in a slot cut in the bushing, prevents the plunger from rotating. As shown in the illustration, this bushing is not tapered on the shank, but is perfectly straight, so, obviously, a special transferring block had to be made to hold it.

Another type of transferring bushing is shown at  $E$ . This bushing has a marked resemblance to that shown at  $B$ , but gives satisfaction because of the character of the work. The hole in the chuck  $a_1$  could be made larger than the diameter of the work, and still the latter would not drop out; thus the difficulty of inserting the work in the chuck is overcome. The hole in the plunger  $b_1$ , to which the chuck is attached is made larger than the teat or threaded part on the work. A spring plunger  $c_1$  is used for inserting the work in the index drilling chuck. Obviously, there are a number of different types of transferring bushings used, but as those shown incorporate the principal features of bushings of this type, it would seem that any further descriptions are unnecessary.

## CHAPTER III

### BURRING ATTACHMENTS

Quite frequently it is found necessary to drill holes in both ends of a piece of work. This cannot be done while the piece is attached to the bar, but necessitates rehandling the work. The Brown & Sharpe Mfg. Co. has designed what is called a "burring" attachment, which is used in connection with its automatic screw machines for drilling and chamfering holes in both ends of the work.

A front view of the burring attachment fastened on a No. 00 Brown & Sharpe automatic screw machine is shown in Fig. 20. Fig. 21 shows a rear view, while Fig. 22 shows plan, end and sectional views.

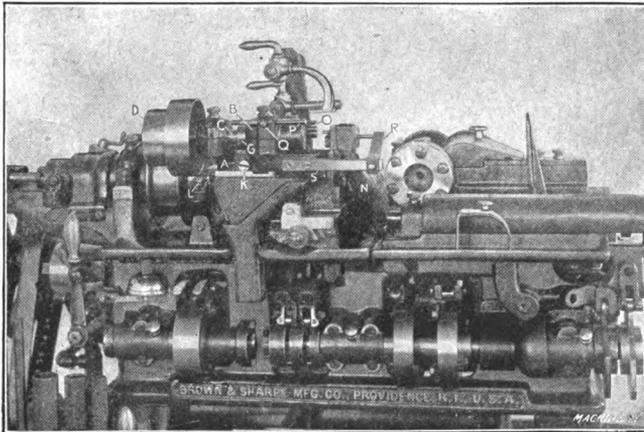


Fig. 20. Front View of No. 00 Brown & Sharpe Automatic Screw Machine equipped with a Burring Attachment

respectively. The attachment consists essentially of a cast-iron base *A*, provided with bearings *B*, in which a spindle *C* is free to rotate, being driven by the two-stepped cone pulley *D*. The bosses *B* are provided with phosphor-bronze sleeves *E* and a thrust washer *F*. The nut *G* is provided for taking care of the end play of the spindle. The burring tool is held in a bushing *H*, fitting in the nose of the spindle *C*, and is furnished with a clamping block *I* acted upon by a set-screw *J*.

This burring attachment can be adjusted to and from the machine by means of the collar-head screw *K*, and the top part of the attachment can be adjusted on its base in a plane with the axis of the spindle, by means of the collar-head screw *L*. The standard workholder *M* is shown in section in Fig. 22, and more clearly in Fig. 26, to which reference should now be made. Here *A* is the chuck, slotted

and spring tempered, *B* the chuck-closing sleeve and *C* the ejector. The chuck-closing sleeve is operated by means of a lever *D*, which is acted upon by pin *E*. To close the chuck, the arm *N*, Fig. 22, is made to dwell in an intermediate position between the work-spindle and the burring spindle, or, in other words, directly in front of the chuck-closing device *O*. The arm *N* is then advanced, when the device *O* forces the sleeve *B* onto the chuck *A*, thus closing the latter on the work.

The chuck *A*, Fig. 26, which is screwed into the transferring block, is opened by means of the pin *E* coming in contact with the end of the rod *P* held in the burring head by a set-screw *Q*, see Fig. 22. When pin *E* comes in contact with rod *P*, the former forces back lever *D*, which, in turn, releases the chuck-closing sleeve *B* and allows the chuck to expand, thus facilitating the removal of the work. The work

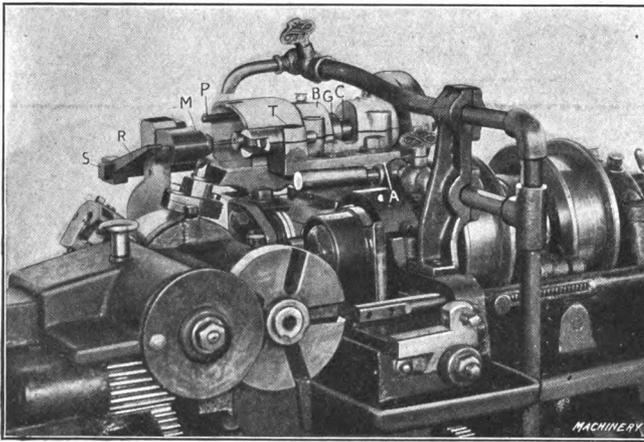


Fig. 21. Rear View of the Burring Attachment placed on a No. 00 Brown & Sharpe Automatic Screw Machine

is removed by means of the plunger *C*, which comes in contact with the finger *R*, Fig. 22, when the arm *N* drops back. This finger is held by a set-screw on a square rod *S*, which, in turn, is fastened to the base of the burring attachment.

Referring now to the view to the right in Fig. 22, the transferring arm *N* is made to dwell in an intermediate position by the combined action of the two cams—transferring and burring—and the two springs *A*<sub>1</sub> and *B*<sub>1</sub>. The transferring lever *C*<sub>1</sub> is fulcrumed on the stud *D*<sub>1</sub> and works in a slot in the connecting link *E*<sub>1</sub>. The link *E*<sub>1</sub>, in turn, is connected to a slotted block *F*<sub>1</sub>, which is fastened to the transferring arm shaft by a cone-pointed set-screw, not shown. The spiral spring *A*<sub>1</sub> bears against the face of the transferring lever *C*<sub>1</sub>, the transferring lever being held to the link *E*<sub>1</sub> by means of the fillister head screw *G*<sub>1</sub> and two check nuts *H*<sub>1</sub>. The spring *B*<sub>1</sub> is used to keep the roll in the lever *C*<sub>1</sub> in contact with the transferring cam, while the spring *A*<sub>1</sub> is used to steady the transferring arm. When the set-screw in the arm *N* comes in contact with the square rod *S*, the lever *C*<sub>1</sub> continues com-

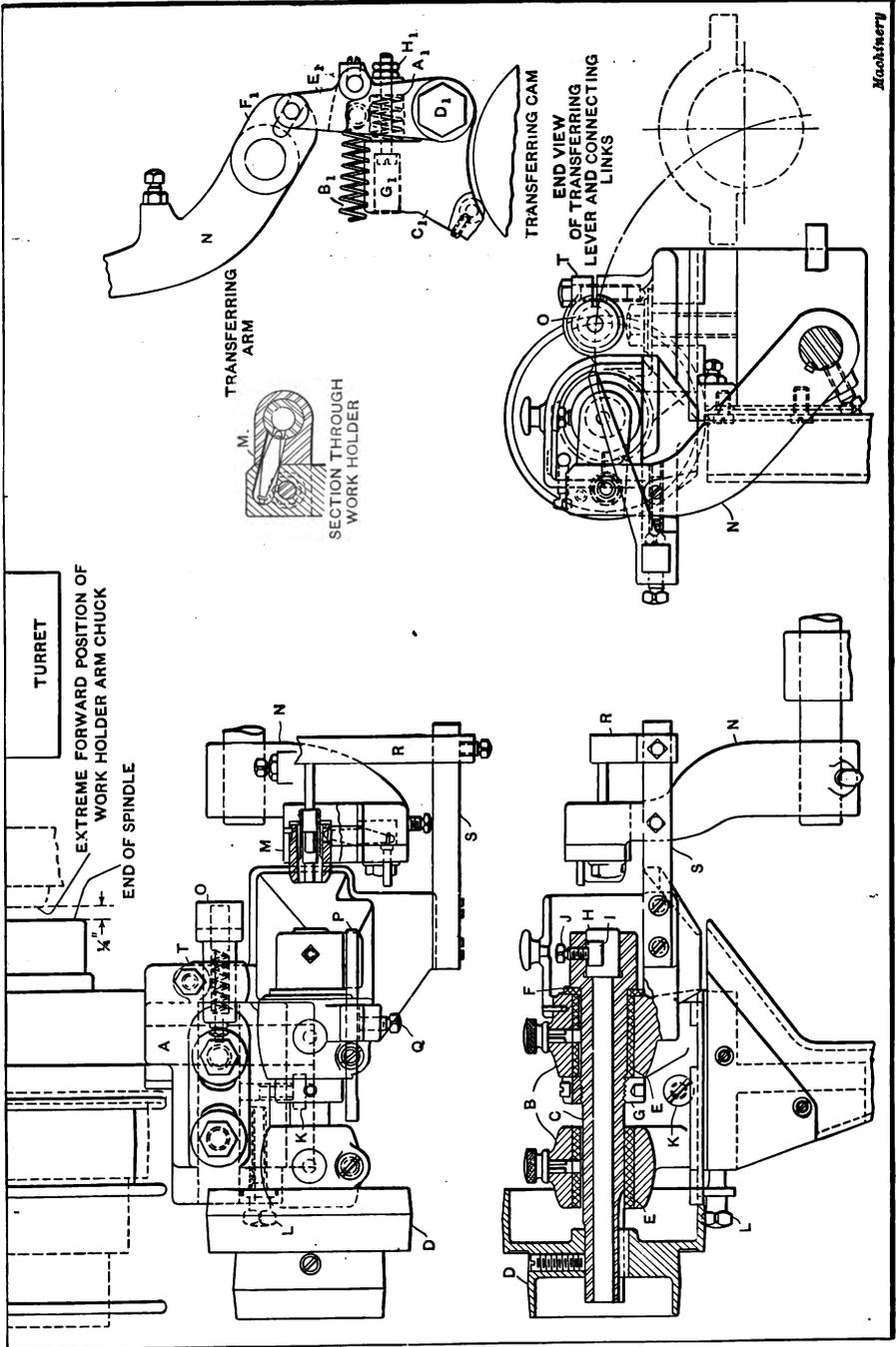


Fig. 22. Plan, Sectional and End Views of the Burring Attachment used on the No. 00 Brown & Sharpe Automatic Screw Machine

Machinery

pressing the spring  $A_1$ , thereby keeping a tension on the arm  $N$  while the burring operation is being performed. The spring  $B_1$  is fastened to the link  $E_1$  and to the tray or bracket-holder for the transferring arm rod. The height of the lobe on the transferring cam governs the angular position of the arm  $N$ .

**Laying out Cross-slide and Lead Cams for Burring Operation**

The same remarks which were made in the previous chapter in regard to laying out cross-slide cams for cross-drilling operations apply

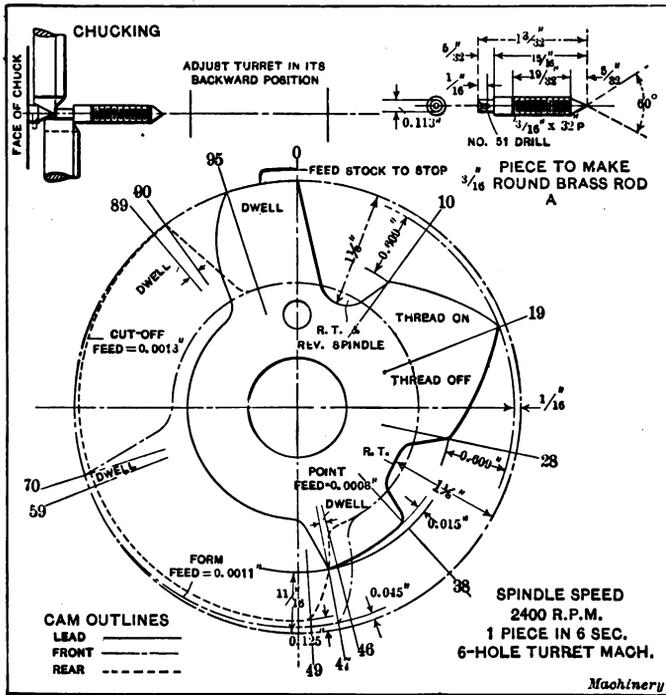


Fig. 23. Lead and Cross-slide Cams for Making a Cone-pointed Screw having a Hole drilled in the Rear End

to the laying out of cross-slide cams for burring operations, it being absolutely necessary to leave sufficient clearance for the arm to ascend and descend to and from the work-spindle. The character of the work and the shape and size of the work-holder also play an important part in regard to the amount of clearance necessary. This, of course, has to be worked out for each individual case. To illustrate clearly the method of designing a set of cams for an ordinary burring operation, we will lay out a complete set of cams for producing the cone-pointed screw shown at  $A$  in Fig. 23. As can be seen a No. 51 drill hole is to be produced in the rear end of this screw, which without the use of this attachment would necessitate rehandling the work and performing a second operation on it.

The cross-slide and lead cams for making this screw are also shown in Fig. 23, where the functions of the various lobes are clearly indicated. It might be mentioned, however, that it was necessary to ad-

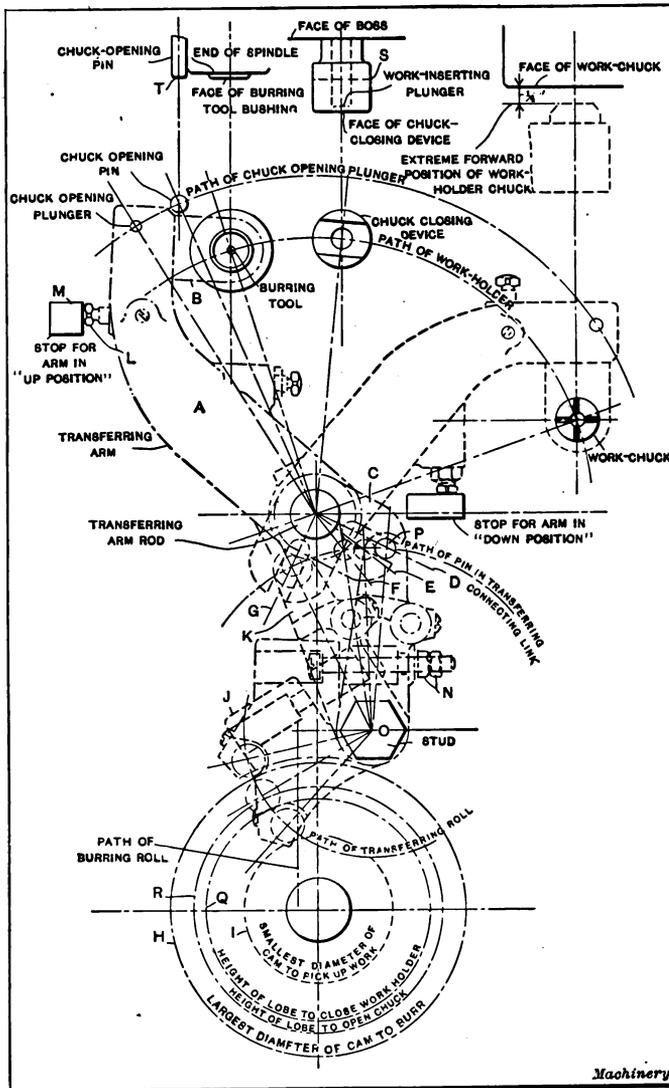


Fig. 24. Diagram used in Determining Rises on the Transferring and Burring Cams

just the turret slide back to the extreme limit to make this long screw in a No. 00 B. & S. automatic screw machine. The time allowed to feed stock is also less than that usually provided, being 5 hundredths instead of 10 hundredths of the cam circumference. The reason for

this is that the turret is not revolved, but is just advanced to gage the stock to length.

**Laying out the Transferring and Burring Cams**

Before proceeding to lay out the transferring and burring cams, a diagram similar to that shown in Fig. 24 should be made. Here the work-chuck, chuck-closing device, burring tool and chuck-opening pin should be laid out in their respective positions, and the angular movement of the arm from one point to the other should be determined.

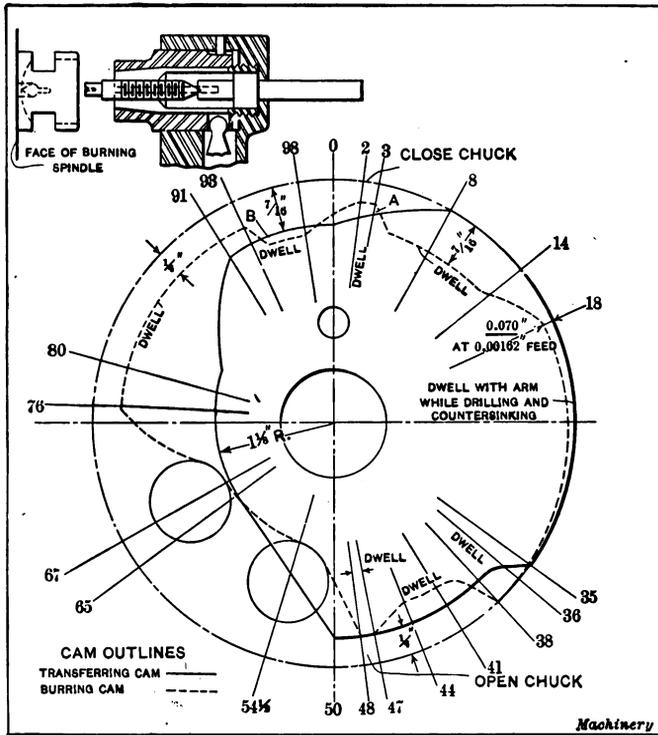


Fig. 26. Transferring and Burring Cams for the Piece shown at A in Fig. 23

A good method for obtaining the angular movement of the arm *A* is shown in Fig. 24. All those parts which are designated by full lines are drawn in; then make a templet of the arm *A*, work-holder *B* and slotted block *C*, on tracing cloth. Now by pivoting this templet on the center of the transferring arm rod, and swinging it around to he various positions, the lines *D*, *E*, *F* and *G* can be drawn which represent the center of the slot in the block *C*, when the arm is swung to the various positions. Next draw the circles *H* and *I*, representing the largest and smallest diameters of the transferring cam, after which a templet of the transferring lever *J* and connecting link *K* should be made on tracing cloth.

As was previously mentioned, the lever *J* should compress the spring *A*<sub>1</sub>, see Fig. 22, when the set-screw *L* touches the square rod *M*, thus steadying the arm during the burring operation. To provide for this the nuts *N* are adjusted, so that the spring *A*<sub>1</sub> will bear the weight of the arm *A*. To proceed, pivot the templet of the transferring lever and connecting link on the center of the stud *O*, swing the templet so that the center of the pin *P* comes in line with the lines *E* and *F*, respectively, and draw circles *Q* and *R* representing the heights of the lobes for closing and opening the chuck. Care should be taken in laying out the lobes to lift the arm from the chuck-closing device to the chuck-opening pin, as the space between the two members is not adjustable. As the spring *A*<sub>1</sub>, see Fig. 22, is compressed further when

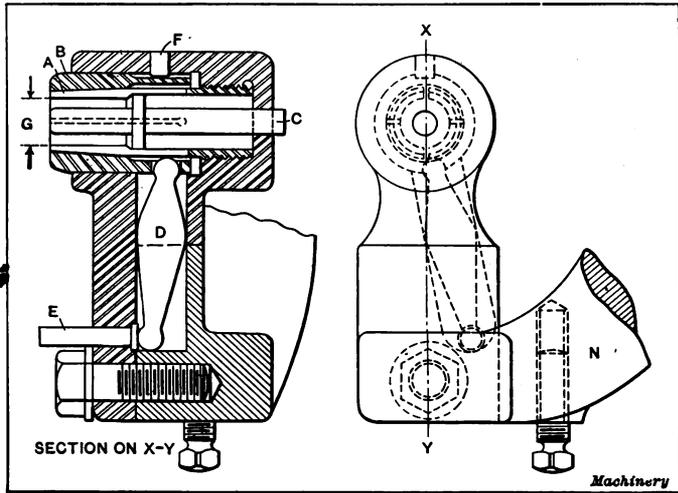


Fig. 26. Standard Work-holder used in Connection with the Burring Attachment

the arm *A* is in the "up position" than when it is in the "down position," it is necessary to start swinging the arm *A* from the work-chuck, and to proceed towards the burring tool. It will be found that the roll in the lever *J* will fall below the largest diameter of the cam, when the arm is in line with the burring tool; this allows the spring *A*<sub>1</sub> to be compressed and thus steady the arm.

To obtain the heights of the lobes on the burring cam, a diagram similar to that shown in the upper view of Fig. 24, should be made. The burring tool should be drawn in position, as well as the work in the work-chuck. The chuck-closing device *S*, and chuck-opening pin *T* are adjustable within a considerable range, but it is best to work from a setting which will be most convenient to the burring tool and work.

The method used in obtaining the heights of the lobes on the advancing cam was described in connection with Fig. 11, Reference Book No. 100 (Part II of this treatise), while the proper procedure to follow in laying out the lobes on the transferring cam in their correct

relation to the lobes on the advancing cam was described in connection with Fig. 12 in the same book. The diagrammatical method used in laying out the transferring and advancing cams for the Nos. 0 and 2 B. & S. automatic screw machines was illustrated in Fig. 14 of Reference Book No. 100.

The transferring and burring cams used in connection with the piece shown at *A* in Fig. 23 are shown in Fig. 25, as is also a sectional view of the work-holder with the work in position. The order of operations for making the piece is as follows:

#### Lead and Cross-slide Cams

Operations	Revolutions	Hundredths
Feed stock to stop .....	12	5
Revolve turret and reverse spindle.....	24	10
Thread on .....	21.6	9
Thread off .....	21.6	9
Revolve turret .....	24	10
Point, 0.015 inch rise at 0.0008 inch feed, dwell 0.10 .....	21.6	9
Form, 0.045 inch rise at 0.0011 inch feed, dwell 0.10 .....	(55.2)	(23)
Cut off, 0.125 inch rise at 0.0013 inch feed, dwell 0.10, and revolve turret four times.....	98.4 + 4.8	41 + 2
Clearance to bring down arm.....	12	.5
<b>Total .....</b>	<b>240</b>	<b>100</b>

#### Transferring and Burring Cams

Operations	Revolutions	Hundredths
Drill and countersink, 0.070 inch rise at 0.00162 inch feed, dwell 0.20.....	48	20
Drop back with piece .....	7.2	3
Rotate to open chuck .....	28.8	12
Dwell on burring cam to open chuck.....	2.4	1
Drop back to eject piece.....	10.7	4½
Drop down to grip work.....	36	15
Dwell with arm before advancing.....	4.8	2
Advance on work .....	21.6	9
Raise arm to close chuck.....	26.4	11
Advance arm to close chuck.....	9.6	4
Close chuck .....	2.4	1
Rotate to burring spindle.....	19.2	8

Referring to Fig. 25, the lobe *A* on the burring cam moves the arm forward to close the chuck, and during this period the transferring arm roll is on the "dwell" on the lobe *B* of the transferring cam. The springs previously referred to steady the arm when in this intermediate position, but on account of this undependable method of steadying the arm, it is not advisable to make a piece in less than three seconds on the No. 00 B. & S. automatic screw machine.

#### Work-holders and Chuck-closing Devices

The standard work-holder furnished in connection with the burring attachment is shown in detail, connected to the arm *N*, in Fig. 26,



The standard chuck-closing device provided with the burring attachment shown at *O*, Fig. 22, is shown more clearly at *A* in Fig. 28. It consists of a body *b* provided with a slot *c* in its front end through which the chuck passes on its transit from the work-spindle to the burring tool. The body *b* is counterbored to receive the spring plunger *d*, which is acted upon by the spiral spring *e*. The plunger is adjusted by means of the check-nuts *f*, and forces the work into the chuck against the ejecting pin *C*, see Fig. 26.

A special locating device used in connection with the work-holder shown in Fig. 27 is shown at *B*, Fig. 28. This device consists of a body *g*, which fits in the clamping bracket *T* on the burring attachment (see Fig. 22). The device is provided with a spring plunger *h* acted

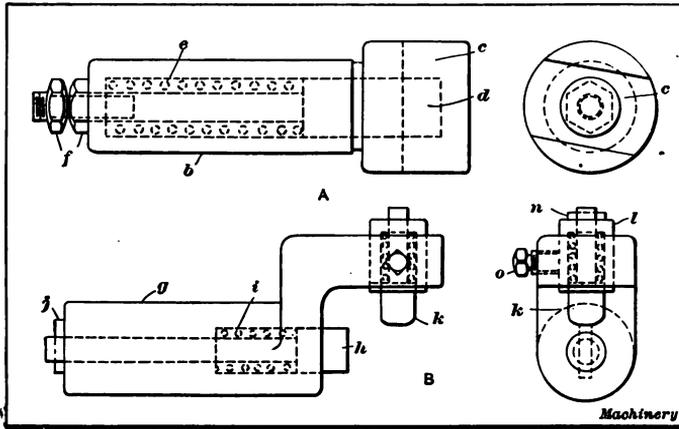


Fig. 28. Standard Chuck-closer, and Device for Locating Work on the Holder shown in Fig. 27

upon by the spring *i*, and is retained in the holder by means of pin *j*. This plunger *h* is used for forcing the work onto the pin *C*, Fig. 27. The plunger *k*, which rotates the work on the work-holder, and thus locates it correctly against pin *D*, is held in a bushing *l* counterbored to receive a spring, and is retained in the holder by means of the pin *n*. The bushing itself is held in the holder by means of the set-screw *o*.

#### Burring Tools and Holders

The type of burring tool and holder used in the burring attachment is governed entirely by the work it is to perform. In Fig. 29 are shown a few representative types of burring tools and their respective holders. *A* is the burring tool used for burring the piece shown at *A* in Fig. 27. This is made from round drill rod, as shown, and is provided with a leader fitting in the work, the cutting face being tapered to the required angle. The type of burring tool and holder used for drilling and countersinking the screw shown at *A* in Fig. 23, is shown at *B*. The holder *a* is made to fit in the burring spindle, and is slotted out to receive the clamping block *b*. A combination drill and counter-

sink *c* of the required shape and diameter is held in this holder by means of a set-screw bearing on the clamping block. The front end of the holder is counterbored to receive the work-holder chuck, and is also provided with two slots *d* which allow the chips to escape.

Another type of burring tool, and the work on which it is used is shown at *C*. In this case the burring tool is a combination holder and tool, being made to fit the hole in the burring spindle. It is also provided with a leader *e* to fit the work, which is turned down on the rear end to suit the holder and held in it by a set-screw as shown.

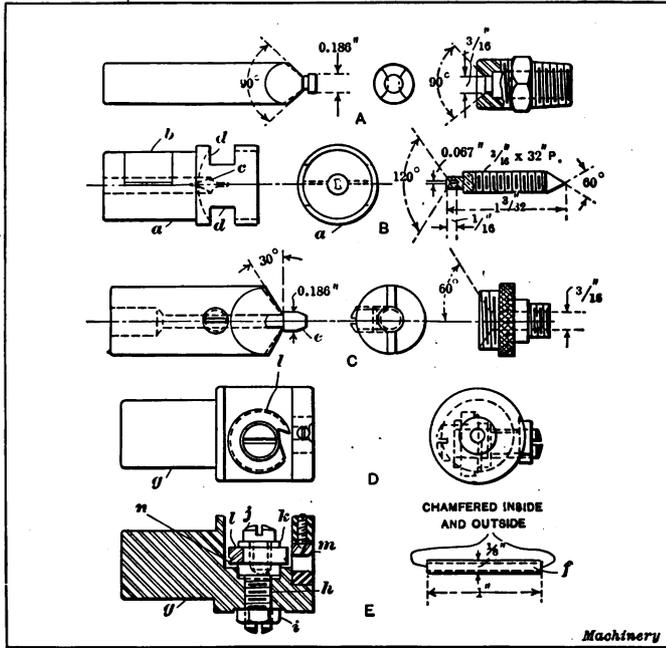


Fig. 29. Various Types of Burring Tools and Burring-tool Holders

Three views of still another type of burring tool and holder are shown at *D* and *E*. This holder and tool is used principally for chamfering the inside and outside of tubing as shown at *f*. The tool used is similar to a circular form tool except that it is of small size. It is held in the holder *g* on a stud *h*, which is threaded into the holder and is provided with a nut *i* for locking it in the desired position. The stud carrying the circular tool is slotted in the lower end, so that it can be adjusted, thus bringing the tool in the correct position to chamfer the inside and outside of the work.

The circular tool *l* is held on the stud by means of a screw *j* and washer *k*. The front end of the holder is provided with a bushing *m*, which fits the external diameter of the work and is held in place by a headless screw as shown. When designing this type of tool, it is

preferable to lay out the work on a large scale, about 10 to 1, and from this obtain the diameter of the tool, and the distance it is to be cut down below the center, so that the tool will clear and not rub, which would tend to produce a poor finish on the work. The depth of the recess  $n$  should only be a few thousandths greater than the length of chamfer required on the work, because the greater the depth  $n$ , the smaller the diameter of the tool, and also the smaller the amount of tool circumference that can be utilized for cutting. From the diagram the location of the stud  $h$  can also be obtained.

#### Speeds and Feeds for Burring

The speeds used for burring when the tools are made from ordinary carbon steel should be similar to those used for drills, a table of which was given in MACHINERY'S Reference Book No. 103, "Internal Cutting Tools for the Brown & Sharpe Automatic Screw Machines." The feeds used when the burring tool is smaller in diameter than  $\frac{1}{4}$  inch should never be greater than 0.003 inch for brass, 0.002 inch for machine steel, and 0.001 inch for tool steel. The feeds should also be decreased near the end of the cut, and a dwell equal to at least three revolutions of the burring tool should be allowed on the burring cam. When the burring tool is  $\frac{1}{4}$  inch or greater, the same feeds as those used for centering tools, given in the article previously referred to, can be used with satisfactory results.

# OUTLINE OF A COURSE IN SHOP AND DRAFTING-ROOM MATHEMATICS, MECHANICS, MACHINE DESIGN AND SHOP PRACTICE

Any intelligent man engaged in mechanical work can acquire a well-rounded mechanical education by using as a guide in his studies the outline of the course in mechanical subjects given below. The course is laid out so as to make it possible for a man of little or no education to go ahead, beginning wherever he finds that his needs begin. The course is made up of units so that it may be followed either from beginning to end; or the reader may choose any specific subject which may be of especial importance to him.

## **Preliminary Course in Arithmetic**

JIG SHEETS 1A to 5A:—Whole Numbers: Addition, Subtraction, Multiplication, Division, and Factoring.

JIG SHEETS 6A to 15A:—Common Fractions and Decimal Fractions.

## **Shop Calculations**

Reference Series No. 18. SHOP ARITHMETIC FOR THE MACHINIST.

Reference Series No. 52. ADVANCED SHOP ARITHMETIC FOR THE MACHINIST.

Reference Series No. 53. USE OF LOGARITHMIC TABLES.

Reference Series Nos. 54 and 55. SOLUTION OF TRIANGLES.

Data Sheet Series No. 16. MATHEMATICAL TABLES. A book for general reference.

## **Drafting-room Practice**

Reference Series No. 2. DRAFTING-ROOM PRACTICE.

Reference Series No. 8. WORKING DRAWINGS AND DRAFTING-ROOM KINKS.

Reference Series No. 33. SYSTEMS AND PRACTICE OF THE DRAFTING-ROOM.

## **General Shop Practice**

Reference Series No. 10. EXAMPLES OF MACHINE SHOP PRACTICE.

Reference Series No. 7. LATHE AND PLANER TOOLS.

Reference Series No. 25. DEEP HOLE DRILLING.

Reference Series No. 38. GRINDING AND GRINDING MACHINES.

Reference Series No. 48. FILES AND FILING.

Reference Series No. 32. SCREW THREAD CUTTING.

Data Sheet Series No. 1. SCREW THREADS. Tables relating to all the standard systems.

Data Sheet Series No. 2. SCREWS, BOLTS AND NUTS. Tables of standards.

Data Sheet Series Nos. 10 and 11. MACHINE TOOL OPERATION. Tables relating to the operation of lathes, screw machines, milling machines, etc.

Reference Series Nos. 50 and 51.

PRINCIPLES AND PRACTICE OF ASSEMBLING MACHINE TOOLS.

Reference Series No. 57. METAL SPINNING.

## **Jigs and Fixtures**

Reference Series Nos. 41, 42 and 43. JIGS AND FIXTURES.

Reference Series No. 3. DRILL JIGS.

Reference Series No. 4. MILLING FIXTURES.

## **Punch and Die Work**

Reference Series No. 6. PUNCH AND DIE WORK.

Reference Series No. 13. BLANKING DIES.

Reference Series No. 26. MODERN PUNCH AND DIE CONSTRUCTION.

## **Tool Making**

Reference Series No. 64. GAGE MAKING AND LAPPING.

Reference Series No. 21. MEASURING TOOLS.

Reference Series No. 31. SCREW THREAD TOOLS AND GAGES.

Data Sheet Series No. 3. TAPS AND THREADING DIES.

Data Sheet Series No. 4. REAMERS, SOCKETS, DRILLS, AND MILLING CUTTERS.

## **Hardening and Tempering**

Reference Series No. 46. HARDENING AND TEMPERING.

Reference Series No. 63. HEAT TREATMENT OF STEEL.

## **Blacksmith Shop Practice and Drop Forging**

Reference Series No. 44. MACHINE BLACKSMITHING.

Reference Series No. 61. BLACKSMITH SHOP PRACTICE.

Reference Series No. 45. DROP FORGING.

## **Automobile Construction**

Reference Series No. 59. MACHINES, TOOLS AND METHODS OF AUTOMOBILE MANUFACTURE.

Reference Series No. 60. CONSTRUCTION AND MANUFACTURE OF AUTOMOBILES.

### Theoretical Mechanics

Reference Series No. 5. FIRST PRINCIPLES OF THEORETICAL MECHANICS.

Reference Series No. 19. USE OF FORMULAS IN MECHANICS.

### Gearing

Reference Series No. 15. SPUR GEARING.

Reference Series No. 37. BEVEL GEARING.

Reference Series No. 1. WORM GEARING.

Reference Series No. 20. SPIRAL GEARING.

Data Sheet Series No. 5. SPUR GEARING. General reference book containing tables and formulas.

Data Sheet Series No. 6. BEVEL, SPIRAL AND WORM GEARING. General reference book containing tables and formulas.

### General Machine Design

Reference Series No. 9. DESIGNING AND CUTTING CAMS.

Reference Series No. 11. BEARINGS. Reference Series No. 56. BALL BEARINGS.

Reference Series No. 58. HELICAL AND ELLIPTIC SPRINGS.

Reference Series No. 17. STRENGTH OF CYLINDERS.

Reference Series No. 22. CALCULATIONS OF ELEMENTS OF MACHINE DESIGN.

Reference Series No. 24. EXAMPLES OF CALCULATING DESIGNS.

Reference Series No. 40. FLY-WHEELS.

Data Sheet Series No. 7. SHAFTING, KEYS AND KEYWAYS.

Data Sheet Series No. 8. BEARINGS, COUPLINGS, CLUTCHES, CRANE CHAIN AND HOOKS.

Data Sheet Series No. 9. SPRINGS, SLIDES AND MACHINE DETAILS.

Data Sheet Series No. 19. BELT, ROPE AND CHAIN DRIVES.

### Machine Tool Design

Reference Series No. 14. DETAILS OF MACHINE TOOL DESIGN.

Reference Series No. 16. MACHINE TOOL DRIVES.

### Crane Design

Reference Series No. 23. THEORY OF CRANE DESIGN.

Reference Series No. 47. DESIGN OF ELECTRIC OVERHEAD CRANES.

Reference Series No. 49. GIRDERS FOR ELECTRIC OVERHEAD CRANES.

### Steam and Gas Engine Design

Reference Series Nos. 67 to 72, inclusive. STEAM BOILERS, ENGINES, TURBINES AND ACCESSORIES.

Data Sheet Series No. 15. HEAT, STEAM, STEAM AND GAS ENGINES.

Data Sheet Series No. 13. BOILERS AND CHIMNEYS.

Reference Series No. 65. FORMULAS AND CONSTANTS FOR GAS ENGINE DESIGN.

Special Course in Locomotive Design Reference Series No. 27. BOILERS, CYLINDERS, THROTTLE VALVE, PISTON AND PISTON ROD.

Reference Series No. 28. THEORY AND DESIGN OF STEPHENSON AND WAL-SCHAERT'S VALVE MOTION.

Reference Series No. 29. SMOKE-BOX, FRAMES AND DRIVING MACHINERY.

Reference Series No. 30. SPRINGS, TRUCKS, CAB AND TENDER.

Data Sheet Series No. 14. LOCOMOTIVE AND RAILWAY DATA.

### Dynamos and Motors

Reference Series No. 34. CARE AND REPAIR OF DYNAMOS AND MOTORS.

Data Sheet Series No. 20. WIRING DIAGRAMS, HEATING AND VENTILATION, AND MISCELLANEOUS TABLES.

Reference Series Nos. 73 to 78, inclusive. PRINCIPLES AND APPLICATIONS OF ELECTRICITY.

### Heating and Ventilation

Reference Series No. 39. FANS, VENTILATION AND HEATING.

Reference Series No. 66. HEATING AND VENTILATING SHOPS AND OFFICES.

Data Sheet Series No. 20. WIRING DIAGRAMS, HEATING AND VENTILATION, AND MISCELLANEOUS TABLES.

### Iron and Steel

Reference Series No. 36. IRON AND STEEL.

Reference Series No. 62. TESTING THE HARDNESS AND DURABILITY OF METALS.

### General Reference Books

Reference Series No. 35. TABLES AND FORMULAS FOR SHOP AND DRAFTING-ROOM.

Data Sheet Series No. 12. PIPE AND PIPE FITTINGS.

Data Sheet Series No. 17. MECHANICS AND STRENGTH OF MATERIALS.

Data Sheet Series No. 18. BEAM FORMULAS AND STRUCTURAL DESIGN.

Data Sheet Series No. 20. WIRING DIAGRAMS, HEATING AND VENTILATION AND MISCELLANEOUS TABLES.

